

Water Injection Effects on Compressor Stage Operation

I. Roumeliotis K. Mathioudakis

Laboratory of Thermal Turbomachines National Technical University of Athens





Water Injection Effect on Compressor Stage Operation

- **Experimental Set-Up**
- **Effect of Water Injection on Stage Characteristic**
- Detailed Aerodynamic Measurements
- **Effect on Stage Power Consumption**
- Conclusions

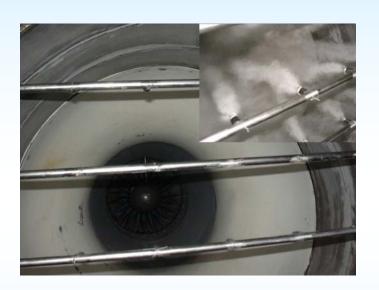


One Stage Axial Compressor

$$N_{C,nom} = 18000 rpm$$

$$\pi_{\text{C,nom}}=1.57$$

$$m_{\text{C,nom}} = 27.5 \text{ kg/s}$$



<u>Impaction Pin Nozzles (Mee Industries)</u>

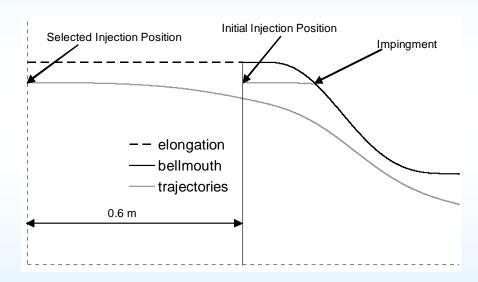
- **Axisymetrically Distributed at Bellmouth Inlet**
- ■Maximum Injected Water Mass Flow: 2%



Bellmouth Configuration

Droplet Trajectories Analysis

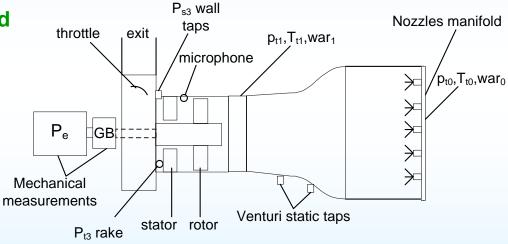
- **Lagrangian Framework**
- **Droplet Evaporation Model**
- Meridional Flow Solver (2D)





Test-Rig Measurements

- 1. The flow rate of water
- 2. The pressure at nozzle manifold
- 3. Compressor Rotational Speed
- 4. Torque of the Shaft
- 5. Ambient Conditions (p_{t0}, T_{t0}, war_0)
- 6. Compressor Inlet Conditions (p_{t1}, p_{s1}, T_{t1}, war₁)
- 7. Inlet Flow Rate (Venturi)
- 8. Compressor Exit Conditions (p_{t3}, p_{s3})
- 9. Oil Thermal Losses





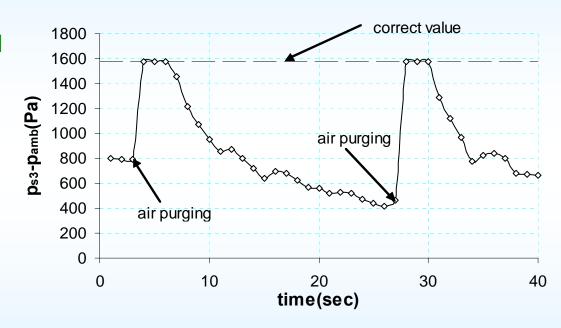
Measurements Considerations

- Pressure Measurement: Potential Plugging of Pressure Holes and Connections due to Droplets
- •Temperature Measurement: Droplets impingement at Temperature Sensors tend to Mask the Flow Temperature
- •Humidity Measurement: Influencing the Measurements used for calculating the Stage Performance Characteristics
- •Unstable Operation Determination: Hot Wire use in Droplet Laden Flow is not Plausible



Pressure Measurements

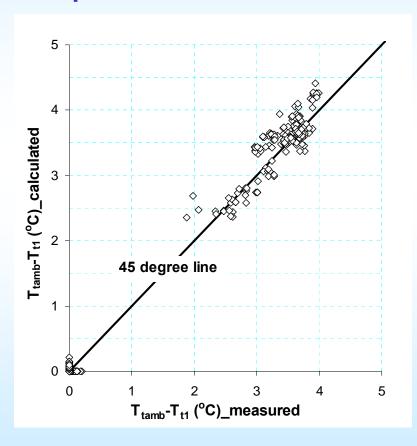
- •Increased Measuring Wall Taps Diameter to 1.5mm
- •Total Pressure Probe of Kiel Type with 3mm Hole
- •Purging System using Pressurized Air and Electronic Vanes
- •Defining of Acquisition Time to 1 sec





Inlet Water to Air Ratio and Temperature Measurement

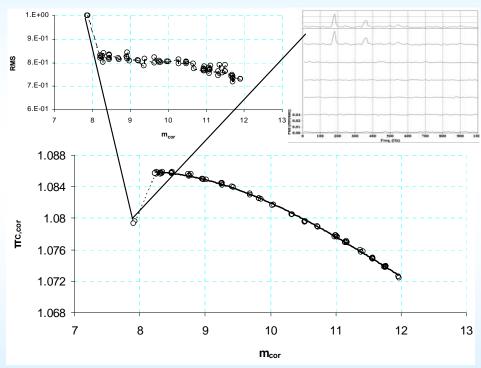
- •Bleeding Air from the Stage Inlet introducing a bent tube facing downstream
- •Humidity Chamber incorporating a RH Sensor and a Pt100 Thermometer
- •Measuring Temperature with a Pt100 Thermometer in the bent tube (insulated)
- •Air Movement Imposing Pressure Difference at the Humidity Chamber





Unstable Operation Determination

- •Unstable operation can be detected by acoustic measurements
- •Use of a Hot-Wire for dry Measurements
- •Microphones used for Droplet Laden Flows



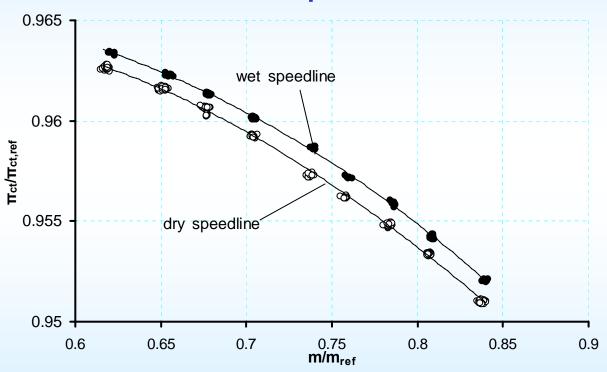


Water Injection Effect on Compressor Stage Operation

- **Experimental Set-Up**
- **Effect of Water Injection on Compressor Characteristic**
- **Detailed Aerodynamic Measurements**
- **Effect on Compressor Power Consumption**
- Conclusions



Raw Effect on Compressor Performance



Tamb = 20.5°C RH=62% mwinj=1%

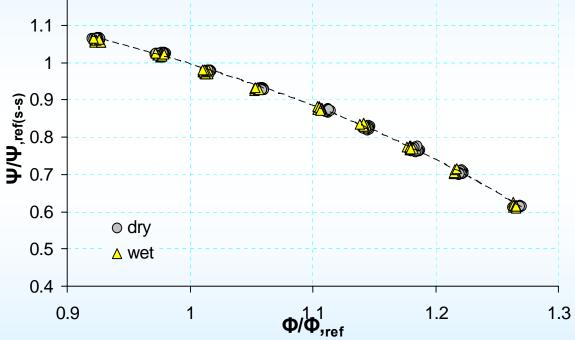


Effect on Pressure Rise Coefficient

•Assuming Incompressible Flow

•Pressure Rise Coefficient:

$$\Psi_{\text{s-s,is}} = \frac{p_{\text{s3}} - p_{\text{s1}}}{\rho_1 \times U_{\text{tip}}^2}$$



Tamb = 20.5°C RH=62% mwinj=1%



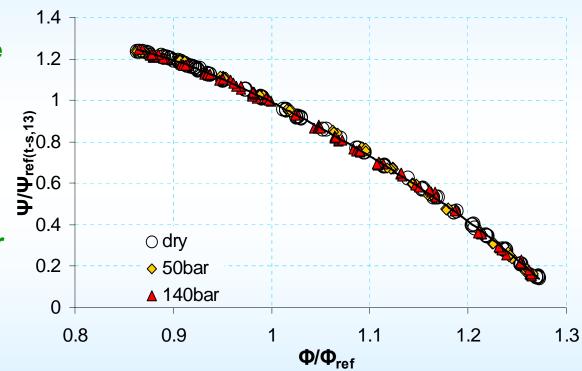
Effect on Pressure Rise Coefficient

- •Assuming Incompressible Flow
- •Manifold Pressure: 50bar

$$m_{winj}/m_{air}=0.6\div0.85\%$$

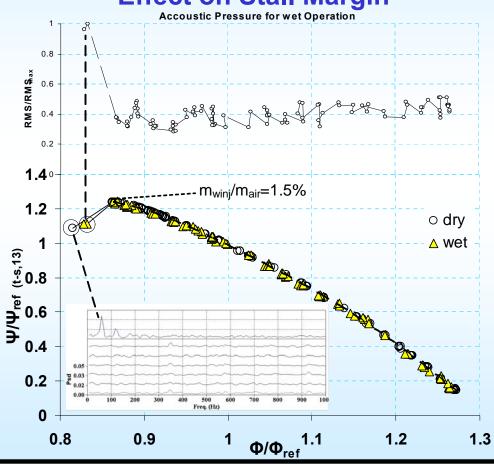
- •MMD=20µm
- •Manifold Pressure: 140bar

•MMD=12μm





Effect on Stall Margin





Water Injection Effect on Compressor Stage Operation

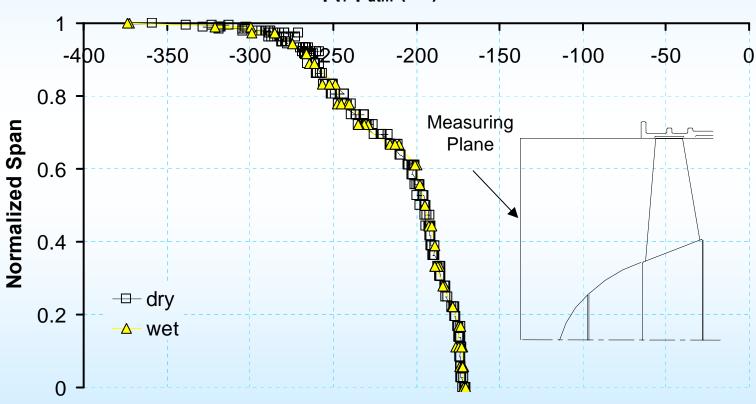
- **Experimental Set-Up**
- Effect of Water Injection on Compressor Characteristic
- **Detailed Aerodynamic Measurements**
- **Effect on Compressor Power Consumption**
- Conclusions



Detailed Aerodynamic Measurements

Inlet Pressure Profile

p_{t1}-p_{atm} (Pa)

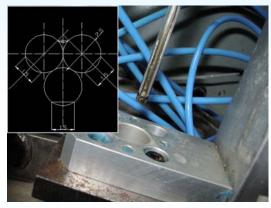


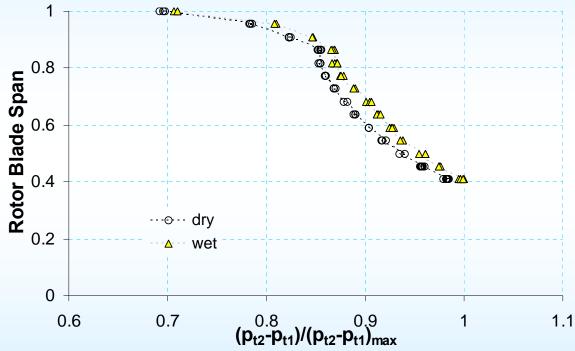
mwinj=1.5%



Detailed Aerodynamic Measurements

Rotor Exit Pressure Profile





mwinj=2%

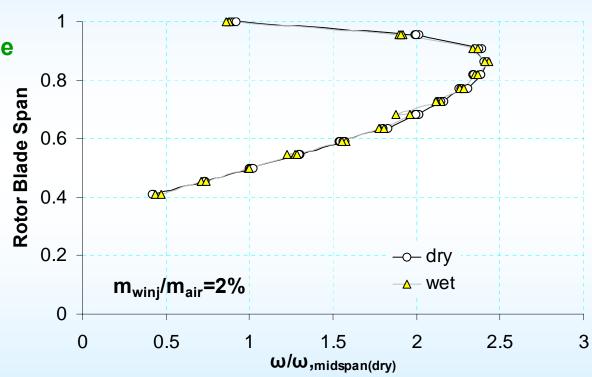


Total Pressure Loss Coefficient Profile

- •Assuming Incompressible Flow
- •Total Pressure Loss Coefficient:

$$\bar{\omega} = \frac{\mathbf{p}_{tR1} - \mathbf{p}_{tR2}}{1/2 \times \mathbf{p}_1 \times \mathbf{W}_1^2}$$

$$\mathbf{p}_{tR} = \mathbf{p}_{s} + \rho \times \frac{\mathbf{W}^{2}}{2}$$



Rotor Blade Span

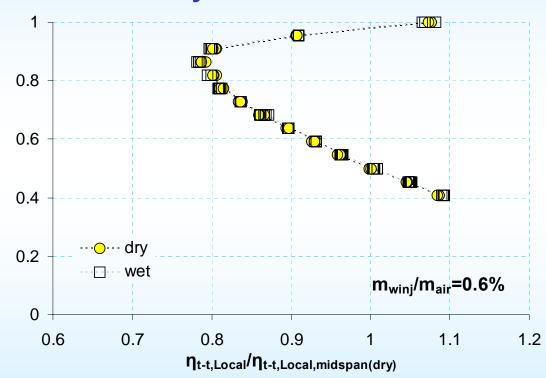


Effect of Water Injection on Compressor Performance

Total to Total Efficiency Profile

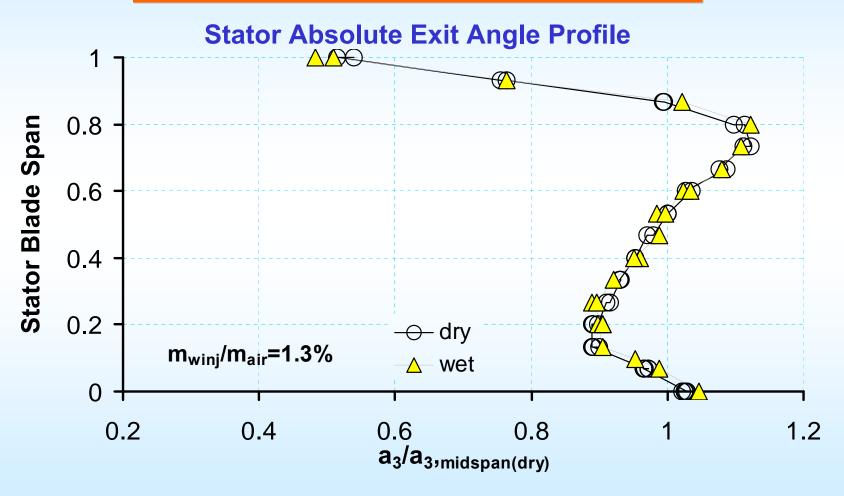
- •Assuming Incompressible Flow
- •Local Total to Total Efficiency:

$$\eta_{t-t,Local} = \frac{p_{t2} - p_{t1}}{\rho_1 \times U(V_{u2} - V_{u1})}$$





Detailed Aerodynamic Measurements



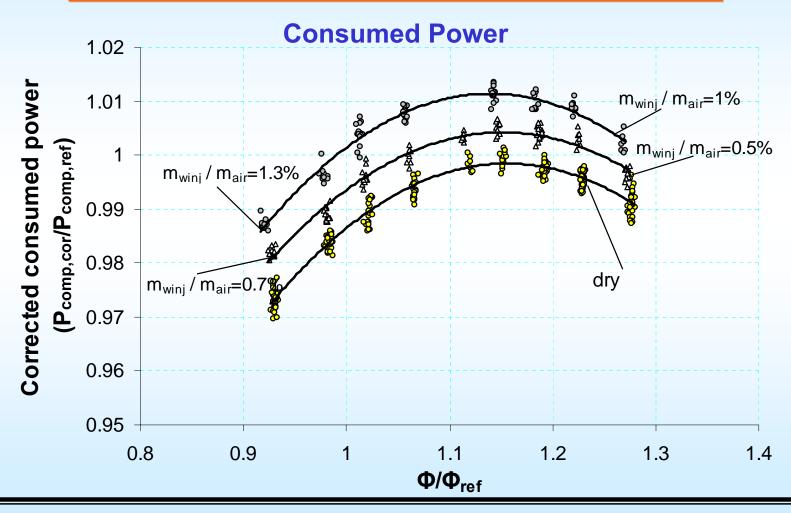


Water Injection Effect on Compressor Stage Operation

- **Experimental Set-Up**
- **Effect of Water Injection on Compressor Characteristic**
- **Detailed Aerodynamic Measurements**
- **Effect on Compressor Power Consumption**
- Conclusions



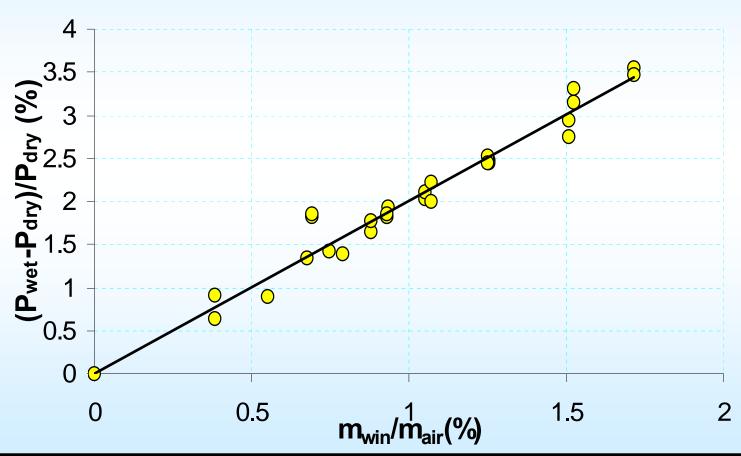
Effect on Compressor Power Consumption





Effect on Compressor Power Consumption

Power Increase



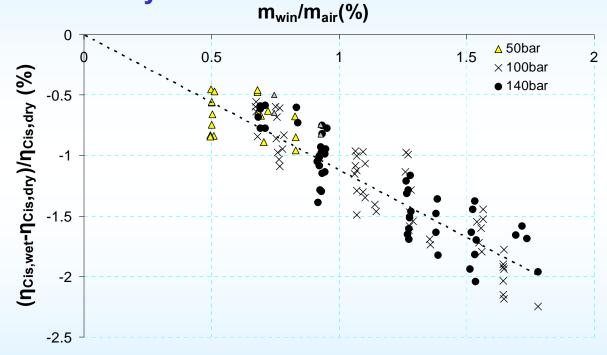


Effect on Compressor Efficiency

Efficiency Decrease

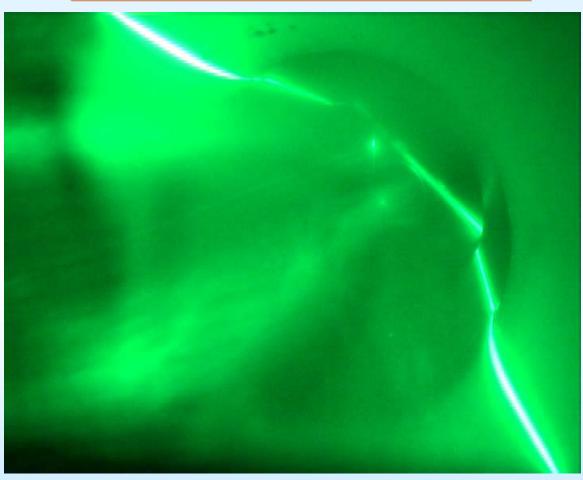
- •Assuming Incompressible Flow
- •Isentropic Efficiency via Mechanical Measurements :

$$\eta_{C,t-t,is} = \frac{\Delta p_{t-t,13}/\rho_1}{P_{COMP}/m_{in}}$$





Preliminary Flow Visualization





Conclusions

- •Special Techniques should be used in order to obtain data from a Wet Compressor
- •The pressure rise coefficient presented no measurable deviation with water injection up to 2%
- •The point where initial stall occurs presented no change with droplet laden flow
- •Aerodynamic measurements indicate that the stage flowfield will not be affected by the presence of droplets for water quantities up to 2%
- •Water injection result to an increase of power consumption
- •The decrease of stage efficiency is a strong function of the water quantity entering the engine and droplet size (from 12µm to 20µm) seems to have no effect



Future Work

- •Further examination of the mechanism resulting to the increase of consumed power is needed
- •Visual examination of droplet behavior at rotor and stator
- Quantification of the losses in correlation to water collection rate on rotor blades
- •Examination of the effect of injection position at power consumption



Acknowledgments

- •The work for this paper has been carried out in the frame of HERAKLITOS program. The program is co-funded by European Social Fund (75%) and National Resources (25%).
- •The cooperation of Mee Industries and Mr T. Mee personally in purchasing the nozzle manifold is gratefully acknowledged



Rotor Relative Angle Turn Profile

